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TONNAGE & COMPOSITION OF LIMESTONE....

QE471.15 L5T6 1939

Tolman, C. E.

REPORT ON TONNAGE AND COMPOSITION OF
LIMESTONE AVAILABLE IN PROPOSED QUARRIES A AND B,
PERMANENTE CORPORATION, AND SUPERFICIAL RESIDUARY CLAY
ON THE PROPERTY OF THE PERMANENTE CORPORATION
SANTA CLARA COUNTY, CALIFORNIA

PART I. (TEXT)

[Faint, illegible text]

C. E. Tolman

J. W. Keenan

Stanford University

June 18, 1939

ALW 2064

QE471.15

L5T6

1939

C. F. TOLMAN
STANFORD UNIVERSITY
CALIFORNIA

June 18, 1939

The Permanente Corporation
1522 Latham Square Building
Oakland, California

Gentlemen:

At your request I submit the results of our sampling of a portion of the Permanente limestone, situated on the southern slope of Bald Peak and on the northern slope of Permanente canyon. The area sampled lies above the 1500 foot level, and also above the mass of Franciscan sandstone and volcanics which separates the great limestone body into two portions. The area sampled covers the Southeast Quarter of Section 18, Township 7. South, Range 2 West and does not include large and easily available bodies of high grade limestone north and east of this area nor the large mass of limestone below the 1500 level on the northern slope of Permanente canyon, nor the mass of limestone south of Permanente Creek. These three additional areas contain large tonnages of high grade "dark" limestone.

The area sampled and the areal extent of the entire body of Permanente limestone is shown on the Location Map accompanying this report.

The present preliminary report is accompanied by the following photographs, maps and tabulations:

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I. Panorama (In Envelope).

Panorama of the south slope of Bald Peak showing the limestone body from Permanente Creek to the top of Bald Peak and the included beds of Franciscan sandstone and volcanics (andesite), trenches dug for sampling, the old lower and upper quarries, and the location of proposed quarries A and B.

II. Maps and Geologic Sections.

- (1) Location map showing extent of Permanente limestone and clay areas sampled. (In roll).
- (2) Geologic map of the area above the 1500 foot contour embracing proposed new quarries A and B. (In roll).
- (3) Sample map of the area of proposed new quarries A and B. (In roll).
- (4) Geologic cross sections showing geology and chemical composition of areas embraced in proposed quarries A and B. The estimates of tonnage and calculations of average value are based on these cross sections. (In envelope).
- (5) Map of Clay Area A. (In roll).
- (6) Map of Clay Area B. (In roll).
- (7) Map of Clay Area C. (In roll).
- (8) Map of Clay Area D. (In roll).

III. Tabulations.

- (1) Tabulations of chemical analyses of limestone to

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data.

- (A) Jack hammer samples.
 - (B) Diamond drill samples.
 - (C) Hand samples.
- (2) Tabulations of analyses of surface clay to date.
- (3) Tabulations of analyses of andesite and associated sandstone formation.
- (A) Upper andesite.
 - (B) Franciscan sandstone and shale along west limestone contact.
 - (C) Interbedded Franciscan sandstone and shale.
- (4) (A) Analyses of bay clays north of the Bayshore Highway (Poland Hand Samples of Clays).
- (B) Logs of wells in area east of Bayshore Highway.
- (5) Tabulations showing tonnage and composition of the Permanente limestone available within the proposed quarry sites A and B. (Text, pp. 17 and 18).
- (6) Tabulations showing tonnage of clay available on the properties of the Permanente Corporation. (Text, p. 20).

Respectfully submitted,

June 26, 1939

Mr. H. P. Davis
Henry J. Kaiser Company
1522 Latham Square Building
Oakland, California

Dear Mr. Davis:

In accordance with the plans outline to you by Mr. Tolman, we have checked over the preliminary report that was given to you on the 19th of June. A few discrepancies were noted, and the corrections to be made are as follows:

(1) Geologic Map -

Along the 1600 foot contour line, near the southern edge of the map, there is an area colored in pink; this area should be colored light blue to denote it as upper light limestone.

(2) Sannie Map -

Lying along the 1600 foot contour line, near the southern edge of the map, there is an area colored pink; this area should be colored light blue to indicate an average calcium carbonate content of 72.04%.

(3) Text of Report -

(A) On page 2, line 21 should read as follows: "3,687,100 tons gross and 2,137,550 tons, etc."

(B) On page 20, the clay tonnage tabulation should read as follows:

	<u>Gross Tonnage</u>	<u>% Coarse Waste</u>	<u>Net Tonnage</u>
Area A	1,050,000	49.5	542,250
Area B	1,755,000	39.5	1,061,000
Area C	787,400	39.6	487,400
Area D	154,700	45.5	76,300
TOTAL	3,687,100		2,137,550

Mr. H. P. Davis
June 26, 1955
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REPORT ON THE LOCATION AND COMPOSITION OF
CERAMIC MATERIALS IN FLOTTING CONCENTRATES FROM THE
SANDWICH MOUNTAINS, AND POTENTIAL RECOVERY OF
THE IRON CONTENT OF THE PERMANENT CONCENTRATE
FROM SANDS COUNTY, CALIFORNIA

Part I, (Cont)

(C) There was no mention made regarding the fact that in diamond drill holes 6 to 9 inclusive, the sludge samples were the only analyses available. When the core analyses have been run, the average grade of the deposit, in the area around these holes, may be changed a slight amount.

Respectfully submitted,

J. V. Newman, Jr.

(A) "High" grade material (B) "Low" grade material
Material

JVN:hp

J. V. Newman, Jr.

This sheet again of Material above the 1000 foot level
(in the proposed quarry) are as follows:

Material	Grade	Quantity
High grade Material	1.311,000	12,000,000
Low grade Material	14,300,000	63,000,000
Total High Material	15,611,000	75,000,000

and the High grade Material is a bed of clay
material and is about 10 feet thick. The amount of
this material is 12,000,000 tons. The chemical composition
is given by Table No. 10. This material can either
be washed or utilized as mix with the clay-bearing portion
of the current run.

The average composition of the material is as follows:

REPORT ON TONNAGE AND COMPOSITION OF
LIMESTONE AVAILABLE IN PROPOSED QUARRIES A AND B,
PERMANENTE CORPORATION, AND SUPERFICIAL RESIDUARY CLAY
ON THE PROPERTY OF THE PERMANENTE CORPORATION
SANTA CLARA COUNTY, CALIFORNIA

Part I. (Text)

SUMMARY OF REPORT

The Permanente limestone available above the lowest level of the two proposed quarries consists of three limestone formations: (1) lower "white" cherty limestone, (2) "dark" high grade limestone, (3) upper "white" cherty limestone.

The average composition and tonnage available of these three types of limestone above the 1500 foot level (in the proposed quarries) are as follows:

	<u>Tons</u>	<u>Composition</u>
Upper light limestone	= 1,341,600	72.04% CaCO ₃
Dark limestone	= 15,320,000	86.21% CaCO ₃
Lower light limestone	= 13,430,000	69.07% CaCO ₃

Interstratified between the lower "white" limestone and the high grade "dark" limestone is a bed of clayey Franciscan sandstone about 30 feet thick. The tonnage of this material is 2,444,000 tons. The chemical composition is given in Tabulation No. 3 C. This material can either be wasted or utilized to mix with the clay-bearing portion of the cement mix.

The limestone formations mentioned above rest on a

thick block of Franciscan sandstone and volcanics (andesite). This formation limits the base of the upper quarry and by its thickness greatly reduces the available tonnage of limestone underlying the sandstone and extending down to the bottom of the canyon of Permanente Creek.

Most of the available limestone above the 1500 foot level can be extracted from the two proposed quarries. If it is desired to utilize all of the limestone above the Franciscan base a subsidiary quarry can be run in from the 1400 foot level to extract the material below the 1500 foot level.

The geologic cross sections have been used to calculate tonnage and average composition of the three limestone formations. They should also be used in laying out the proposed quarries.

Finally, only a portion of the available tonnage of high grade "dark" limestone on the Permanente property will be extracted from the proposed quarries. The extent of the entire Permanente limestone body is shown on the Location Map attached to this report.

Clay.

3,697,100 tons gross and ^{2,137,550}~~2,325,500~~ tons after coarse is deducted of residuary clay capping most of the property of the Permanente Corporation has been sampled and analyzed, and the analyses are attached herewith.

Unlimited deposits of bay clays are available in the swamp lands of the San Francisco Bay eight miles from the property of the Corporation and clays of similar character occur under a thin layer of overburden between the bay and Bayshore Highway.

PERMANENTE FORAMINIFERAL LIMESTONE

The limestone body herein described is the largest known deposit of foraminiferal limestone of Franciscan

Age. Exposures of this type of limestone were mapped by A. C. Lawson in the San Mateo and Tamalpais quadrangles¹⁾, by J. C. Branner in the Santa Cruz quadrangle (including the Permanente deposit)²⁾, and the continuation of this zone was mapped by John van Steen Tolman south of Guadalupe Creek and on Calero Creek south of Calero damsite in the New Almaden quadrangle.³⁾ Limestone occurs as lenticular masses in this zone nearly one hundred miles long.

By far the largest and most important of these deposits is the Permanente limestone mass. Detailed drilling and sampling has shown that the Permanente limestone is divided into three distinct units: (1) the lower "white" limestone, also designated in the field as cherty white limestone, averaging 200 feet in thickness as shown in the geologic cross sections; (2) the central formation of "dark" limestone, averaging 200 feet in thickness, also called blue limestone on account of the color of weathered surfaces, colored by hydrocarbon residues; it contains

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- 1) U.S. Geol. Surv. Geologic Atlas, San Francisco Folio, No. 193, p. 22, 1914.
 - 2) U.S. Geol. Surv. Geologic Atlas, Santa Cruz Folio, No. 163, 1909.
 - 3) Geological Report on the Calero, Almadens, and Guadalupe Damsites, Plate VIII, 1934.

only a small amount of chert; (3) the upper horizon of "white" limestone with much interbedded chert, similar in character and composition to the lower horizon of "white" limestone.

The base of this series is a wedge-shaped mass of Franciscan volcanics and sandstones, the uppermost contact of which lies in the vicinity of the 1500 foot level and will form the bottom of the proposed quarry B. Below the Franciscan inclusion the limestone series is repeated by thrust faulting, and a large additional tonnage of available limestone not included in this report occurs below the 1500 foot contour down to Permanente Creek and also on the mountain slopes south of the creek. The investigation of the details of this faulting and of the structure of the entire mass of limestone has not as yet been completed and will be discussed in the final report and depicted in the final cross sections. The accompanying cross sections show the structure in so far as it affects the proposed quarries A and B.

An interesting feature discovered by detailed sampling is the uniformly high grade of the "dark" limestone and the uniformly lower grade of the two "white" limestone members carrying interbedded chert. This relation is constant and geologic structure was determined by lithology (color of formation), chemical composition, and by the attitude of the beds shown by dips and strikes. It seems

probable that conditions which developed the small amount of hydrocarbons in the enclosed basin in which the "dark" foraminiferal limestone was laid down were unfavorable for the deposition of abundant chert, while in the absence of hydrocarbons the micro-organisms secreting silica and the foraminifera secreting calcium carbonate were both active.

The separation of the deposit into one high grade (in calcium carbonate) and two lower grade members is of economic importance. As shown on the geologic cross sections the "dark" limestone and the "white" limestone can be quarried separately, and any mixture desirable can be sent to the cement mill.

If the "white" limestone is used in large amounts the chert must be separated from the limestone. This can be accomplished in part by rejecting the larger chert beds in quarrying and nearly complete elimination of chert can be accomplished by flotation. Mixing of high grade "dark" limestones with the lower grade "white" limestone might make it possible to manufacture cement for many years without recourse to flotation, and, in any case, probably only the "white" limestone, and possibly only a portion of the "white" limestone, will be treated by flotation.

As the important geologic features are depicted on the maps and cross sections, these are described briefly in the following paragraphs with emphasis laid on the features of practical importance in regard to quarrying

and mixing for cement. Further technical geologic description will be reserved for the final report.

DESCRIPTION OF PANORAMA OF SOUTHERN SLOPE
OF BALD PEAK TO PERMANENTE CREEK (TAKEN JUNE 13, 1939).

This panorama shows Trenches No. II, III, IV, and V and diamond drills at Holes No. 9 at right, 8 at center, and 6 at left. The wedge of Franciscan sandstone and volcanics is shown in the center ground and widens greatly to the right, that is, towards the east, cutting out both the upper and lower limestone bodies east of the two old quarries. Hence, the continuation of the limestone beyond the proposed quarries lies to the northeast of the present Upper Quarry. This relation is shown on the Location Map.

The photograph was taken on the high ridge south of Permanente Creek, and hence the limestone south of the creek is not shown on the photograph.

DESCRIPTION OF GEOLOGIC MAP.

The geologic map of the proposed quarries A and B of the Permanente Corporation shows the areal extent of the geologic formations enumerated in the introductory paragraph. On it are plotted the numerous strikes and dips registering the attitude of the beds that were measured during this examination. As much of the area is covered with brush and soil, trenching was necessary to expose the limestone formations.

The outcrop areas of the "dark" limestone with high calcium carbonate content and low in chert are shown in blue. There are two areas of this formation shown on the map, a minor strip parallel to the main fault zone (also described as the "boundary fault") which cuts and terminates the Permanente limestone on the northwest, and the main outcrop, approximately one half the area mapped, bounded on the northwest by the "breccia fault".

This body of high grade limestone makes the deposit commercially valuable, and without it the two "white" cherty members would probably not be of commercial value.

The "dark" limestone surrounds the outcrop area of upper "white" cherty limestone, and this in turn encloses the upper Franciscan andesite. This pattern of older beds surrounding younger members is a graphic representation of the main structure of the limestone body above the 1500 foot level; namely, a syncline or trough plunging towards the east (see cross sections).

The "upper andesite", colored in green at the right center of the area mapped, widens rapidly towards the east of the quarry area and joins the main body of Franciscan andesite and sandstone shown on the map. This thickening of the volcanic members shown at the bottom of the map cuts out the limestone to the east of the area mapped.

The lower cherty limestone, colored in pink, lies south of the "dark" limestone and above the main included mass of Franciscan andesite and sandstone. It is brought up again

northwest of the main body of "dark" limestone by the "breccia fault". The narrow band of "dark" limestone mentioned previously borders the lower cherty limestone on the northwest and is completely cut off by a great "boundary" fault zone, the hanging wall of which is shown on the map.

STRUCTURAL CROSS SECTIONS.

The geologic structure is shown on vertical cross sections which are usually constructed from formational boundaries and strike and dip observations plotted on the geologic maps. In addition to these data we have used the following information:

(1) Core samples obtained from ten diamond drill holes which show the character of rock and attitude of beds in each hole.

(2) The logs of nine diamond drill holes put down by the Santa Clara Holding Company and chemical analyses of this material.

(3) The logs of three churn drill holes bored by the California Portland Cement Company and chemical analyses of sludge samples.

(4) Jack hammer samples. These holes were from 12 to 20 feet deep and were spaced at 50 foot intervals. The dry cuttings were collected, and character of each sample shows type of limestone. These samples were analyzed.

In plotting all the above data it was discovered that the

sedimentary sequence - namely, (1) the lower "white" cherty limestone, (2) the intermediate "dark" non-cherty limestone, and (3) the upper "white" cherty limestone - was well established. Color, chemical analysis and occurrence all gave an identical sequence of formations. The maps and cross sections showing chemical composition are identical with the maps and cross sections on which geologic formations are plotted.

This result was both surprising and satisfactory as it was feared, before the detailed studies were carried on, that the chert might be distributed erratically throughout the limestone sequence and that large bodies of homogenous high grade material might not exist.

The definite formational boundaries between these three types of limestone also assisted in determining the structure of the deposit, and, therefore, the accompanying geologic cross sections are far more accurate than could have been made from geologic observations at ground surface alone, no matter how detailed such observations might be.

Structural Cross Section through Trench No. II.

This section shows the geologic conditions near the eastern margin of the proposed quarries and also the position of the upper andesite exposed where the trench intersects the road to the Permanente Clubhouse. Diamond Drill Hole No. 7 was put down in the center of this volcanic

material. The analyses of this "upper andesite" are tabulated. It appears that it can be incorporated in the clay of the cement mix if the clay is low in magnesia and silica.

The bulk of the material shown in this section is high grade "dark" limestone which averages a little over 200 feet in thickness. A band of Franciscan sandstone which contains a little andesite in Drill Hole No. 1 averages about 40 feet thick in the section, thinning towards the north. The analyses of this interbedded layer of sandstone is shown in Tabulation No. 3.

If this material can be used as a portion of the clay constituent of the cement mix, it will not be necessary to waste it in quarrying.

Only a small thickness of the upper "white" limestone is shown in this section.

The lower "white" limestone has been penetrated to a depth of 230 feet in Hole No. 5 and 223 feet in Drill Hole No. 6 which did not reach to the underlying Franciscan sandstone. The position of the main block of andesite and sandstone will be indicated more accurately after Drill Holes No. 8, 9 and 10 reach this material. It is hoped, therefore, that these holes will be continued until the underlying Franciscan material is encountered.

The upper andesite shown in Drill Hole No. 7 lies in the faulted syncline. This syncline is the main structural feature of the limestone body and was mentioned in the

description of the geologic map. At the south end of the section the limestone is folded, and the anticline is dragged into the overturned position by the thrust fault at the contact with the main Franciscan block.

Cross Section through Trench No. III.

This cross section shows the lower cherty member 150 to 200 feet thick, the interbedded Franciscan layer 15 to 50 feet thick, and the maximum thickness of the "dark" non-cherty member varying from 220 feet to nearly 300 feet in this cross section.

The bulk of the material south of Drill Hole No. 2 encountered in this portion of the quarry will be the high grade "dark" limestone.

The main syncline shown in the cross section has flattened into a gentle structure. The overturn along the thrust fault is pronounced. The main fault which cuts off the limestone body lies just north of the section, and the parallel "breccia fault" is shown on the north end of the section.

Cross Section through Trench No. IV.

In cross section No. 4 the main boundary fault is shown at the north and the parallel "breccia fault" some 300 feet to the south. The high grade "dark" limestone is from 180 to 200 feet in this section and is separated from the underlying "white" limestone by the bed of Franciscan sandstone (shown in all the cross sections) 15 to

30 feet thick. The average thickness of the lower limestone as determined from the log of Drill Hole No. 5 is about 200 feet.

In this section the high grade limestone forms a belt of nearly 200 feet in thickness, approximately parallel to the ground surface, extending from the cliffs just above the main Franciscan contact to a point 290 feet south of the property line.

The main synclinal structure has flattened out into two gentle undulations approximately parallel with the ground surface.

This section is extended across Permanente canyon to the base of the limestone south of Permanente Creek. The structure of the limestone members is indicated by plotting the contacts between the lower "white" limestone, the "dark" limestone, and the upper "white" limestone. The structure of the lower body will be portrayed in detail in the final report.

Cross Section through Trench No. V.

This interesting cross section shows the "boundary fault" at the north end of the section and the "breccia fault", also shown in the cross section through Trench No. IV. It also shows a local compression of the main syncline and the universal overturning of strata at the Franciscan sandstone contact at the base of the proposed

quarry. The interstratified layer of Franciscan sandstone shown in all the cross sections feathers out at the south end of the section. The "dark" high grade limestone in this section of the quarry will not average over 50 feet in thickness and will comprise the near-surface material.

To quarry the large body of lower "white" limestone it will be necessary either to utilize or to waste the interbedded Franciscan sandstone layer.

The limestone is entirely out off about 100 feet south of the property line by the "boundary fault", and from this point for a distance of 190 feet southerly the "dark" limestone constitutes a thin surface cap. Under this cap and extending to the "breccia fault" 360 feet south of the "boundary fault", a thickness of about 200 feet of the underlying "white" cherty limestone only is available for quarrying.

Cross Section through Drill Holes W-1 and DD 2, 5 and 6.

This cross section is approximately at right angles to the cross sections previously described and may be considered a longitudinal cross section roughly parallel to the northerly quarry faces.

This cross section brings out the continuity of the included stratum of Franciscan sandstone which separates the "dark" limestone from the underlying "white" cherty limestone. It shows the cutting out of the "dark" limestone at the west end of the section by the "breccia fault".

The Practical Value of the Cross Sections.

The north-south cross sections are used to determine tonnage and average value of the quarry above the 1500 foot level. All the material above that level can be worked out by two quarries, one at about the 1500 foot level, and the second at the 1700 foot level.

These cross sections can serve as a guide if it is desired to mine exclusively the high grade "dark" limestone for a number of years and for the laying out of the quarry to get any desired percentage mixture of the "dark" and the "white" limestone.

The interbedded layer of Franciscan sandstone will either be wasted or used in the clay mix. This tonnage, therefore, can be added to the available clay supply. In any case, it must be deducted from the limestone tonnage.

Due to request for prompt transmission of this report, these sections were not reduced to the same scale as the geologic map.

SAMPLING

Three sampling methods were used in the exploration of the limestone body at Permanente; namely, diamond drilling, jack hammer drilling and milled hand channels across exposed outcrops. It was first thought that the hand channel sampling would be important. However, two main obstacles were encountered in hand sampling: (1) the scarcity of exposures that could be fairly sampled

and (2) differential weathering of limestone which caused the chert to protrude on the rock surfaces. The latter caused silica to be added to the sample unless extreme care was maintained.

The jackhammer sampling was developed to supplement the hand channel samples. Holes were drilled at fifty foot intervals along each of the five trenches that were cut down to bedrock. The holes varied in depth according to the type of rock drilled. Twenty foot holes were drilled where the rock was homogenous and did not cave badly, and the average hole was between twelve and sixteen feet deep.

Each hole was divided into four foot sample intervals, and during drilling all cuttings were blown from the hole by means of a blowpipe and drillings for each four feet constituted a sample. The cuttings were collected by means of a powder box fitted with the necessary holes and gaskets so that the drillings would be blown into the box container. All drilling was done without water, and the cuttings were easily lifted by the blowpipe from these comparatively shallow depths.

The diamond drill sampling is primarily dependent upon continuous sludge return. The broken and laminated character of the rock rarely allows more than 25% core recovery. Continuous sludge return was obtained by cementing the hole whenever the water was lost during drilling, and further, by cementing at the end of each shift. All of the cuttings during the drilling of each five foot run were collected

and washed in a large tub, dried, quartered and preserved as a sample.

All of the core that was recovered was placed in individual core boxes and after examination was split into two equal parts. One part was crushed, pulverized and analyzed, while the other was permanently filed in a core box.

Where appreciable core was recovered, the core and sludge analyses were combined according to the percent of core recovered.

TONNAGE ESTIMATES

Method of Calculation.

The tonnage of the limestone was calculated as follows:

Planimeter measurements were made of each formation. Each cross sectional area was multiplied by one half the distance between adjacent trenches for section 5 and 4. The tonnage represented by Trench II was determined by multiplying the areas by a width of 386 feet. The tonnage represented by Trench V was determined by multiplying the planimeter area by 236 feet, and the triangular shaped additional area to the west was determined by multiplying one half the planimeter area of Trench V by 300 feet.

Tonnage of Formations.

1700 - 1900 Quarry:

Upper light limestone	=	577,000 tons
Dark limestone	=	8,433,000 tons
Lower light limestone	=	<u>6,665,000 tons</u>
Total limestone	=	15,675,000 tons
Upper Andesite	=	131,000 tons
Franciscan sandstone & andesite	=	873,000 tons

1500 - 1700 Quarry:

Upper light limestone	=	764,600 tons
Dark limestone	=	6,887,000 tons
Lower light limestone	=	<u>6,765,000 tons</u>
Total limestone	=	14,416,600 tons
Franciscan sandstone & andesite	=	1,571,000 tons

Total Both Quarries:

Upper light limestone	=	1,341,600 tons
Dark limestone	=	15,320,000 tons
Lower light limestone	=	<u>13,430,000 tons</u>
Total limestone	=	30,091,600 tons
Upper andesite	=	131,000 tons
Franciscan sandstone & andesite	=	2,444,000 tons

CALCULATION OF CHEMICAL ANALYSES

The average grade of the limestone was derived by weighting the analyses according to the thickness of the beds penetrated by diamond drill holes and intersected by jack

hammer samples.

The analyses of diamond drill holes were averaged for 25 foot intervals except where marked variations were noted. These results were plotted on the cross sections.

The following composition was derived for all limestone above the 1500 foot level:

Upper light limestone	=	72.04%	CaCO ₃
Dark limestone	=	86.21%	CaCO ₃
Lower light limestone	=	69.07%	CaCO ₃

CLAY DEPOSITS

As stated in various communications addressed to this Corporation, various types of clay are available, and the available tonnage of two types is practically unlimited.

These available clay deposits are as follows:

(1) The residuary clay mantle that overlies the bedrock capping most of the property of the Permanente Corporation. Five areas, namely, Areas A, B, C, D and E, have been bored, sampled, and tonnage estimates made. A portion of this large tonnage is of special value for initial operations on account of more favorable chemical composition as shown on the tabulated analyses and because certain of the stripped areas will not be conspicuously visible when viewed from the valley.

A part of Area B is superficially altered Santa Clara formation, the bedrock of which is clay cemented wash conglomerate. If samples of this area are satisfactory, it is probable that deep cuts can be made in the Santa Clara

formation and large additional tonnage can be provided in the immediate vicinity of the plant.

An unlimited tonnage of clay of constant value can be obtained by dredging cheap marshland of the San Francisco Bay or by mining in pits a similar clay which is covered by a shallow overburden and extends approximately up to the Bayshore Highway.

The data available in regard to these deposits is limited to a preliminary report made to the Permanente Corporation by Mr. J. F. Poland. He states:

"Area 1. The marshlands and sloughs on the southwest side of San Francisco Bay will furnish an inexhaustible supply of blue clay. Eight samples of this clay have been collected and turned in to your Permanente laboratory for analysis. This area has the advantages of cheap land and no overburden. It is eight miles from your property, however.

"Area 2. The Bayshore Highway area will supply clay of essentially the same quality as that obtainable from the marshlands. ...Land values will be higher than in Area 1, but the source of supply will be six to seven miles from your plant. Test boring of any property is recommended before purchase. A power or hand auger outfit will furnish the cleanest samples.

"Development operations in this area would probably require the removal of 6 to 10 feet of superficial soil.

This region is not planted to fruit trees and should be

lower priced than the land in Area 3, particularly east of the Bayshore Highway. The Sunnyvale Air Base occupies much of the central part of this area, but there is an extensive region available east of the Air Base property."

A copy of the logs of wells situated within Area 2 between the Bayshore Highway and the bay appears in Tabulation 4 B, and the analyses of the samples of the slough material taken by Mr. Poland appears in Tabulation 4 A.

A study of the tonnage estimates and chemical analyses indicates that there are large and sufficient deposits of various types of clay available, and the engineers in charge of the plant can select the type of deposit most satisfactory under the particular conditions that exist at Permanente.

CLAY TONNAGES

The clay tonnage was determined by multiplying the average depth of the clay samples times the horizontal area in square feet.

	<u>Gross Tonnage</u>	<u>% Coarse Waste</u>	<u>Net Tonnage</u>	
Area A =	1,050,000	48.5	553,550	542,500
Area B =	1,755,000	39.5	1,061,000	
Area C =	737,400	39.6	457,400	
Area D =	<u>134,700</u>	43.3	<u>765,750</u>	76,500
TOTAL =	3,697,100		2,865,500	2,118,000 2,120,500

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JACKHARTN SAMPLES

ASSAY OF LGA
JACKRABBIT SAMPLES

NO. HOLE
LOCATION
DESCRIPTION

PAGE 9

SAMPLE NUMBER	WEIGHT OF CORE	ASSAY OF CORE			WEIGHT OF SLUDGE	ASSAY OF SLUDGE			CALCULATED ASSAY		
		CaCO ₃	SiO ₂	Fe ₂ O ₃		CaCO ₃	SiO ₂	Fe ₂ O ₃	CaCO ₃	SiO ₂	Fe ₂ O ₃
JR	71A	88.6	8.0	0.7							
	71B	94.6	1.6	---	2.9						
	71C	84.5	1.5	---	1.2						
	71D	81.8	8.8	1.1							
	71E	89.7	9.0	0.7							
	72A	61.0	26.2	2.0							
	72B	86.9	2.1	1.0							
	72C	76.0	21.0	1.0							
	72E	78.1	20.2	1.1							
	73A	83.0	13.6	1.4							
	73B	84.1	14.6	1.2							
	75C	66.0	11.1	1.2							
	75D	88.5	2.5	0.8							
	75E	86.8	11.5	1.4							
	72A	88.0	23.0	2.4	0.7						
	72B	73.0	22.0	1.6							
	74C	71.0	26.2	1.8							
	74D	69.7	10.2	1.2							
	74E	87.6	10.7	1.1							
	75A	78.5	17.7	1.7							
	75B	78.0	22.1	1.0							
	75C	67.5	20.7	1.1							
	75D	61.8	25.6	1.8	0.3						
	76A	73.8	26.1	1.0							
	76B	78.3	18.2	1.5							
	76C	73.8	22.6	1.5							
	77A	82.4	15.0	0.8	0.8						
	77B	77.3	20.3	1.1							
	77C	74.3	23.4	1.1							
		0.0			HgO						
	77D	39.8	61.5	3.4	0.0						

ASSAY LOG
JACKHAMMER SAMPLES

NO. HOLE
LOCATION
DESCRIPTION

Page 6

SAMPLE NO.	WEIGHT OF CORE			WEIGHT OF SLUDGE			CALCULATED ASSAY			
	CaCO ₃	SiO ₂	Fe ₂ O ₃	CaCO ₃	SiO ₂	Fe ₂ O ₃	CaCO ₃	SiO ₂	Fe ₂ O ₃	MgCO ₃
49A	Tr.	89.8	8.7							
	CaO									MgO
49B	8.8	85.8	10.7							0.8
	CaO									MgO
49C	2.0	78.8	22.8							1.4
	CaO									MgO
50A	0.8	88.2	9.4							0.7
50B	Tr.	85.5	14.8							MgO
50C	77.8	20.3	2.5							0.7
	CaO									MgO
51A	1.7	82.6	14.7							0.9
	CaO									MgO
51B	0.8	86.9	9.6							0.8
51C										MgO
	3.0	80.6	15.6							0.9
	CaO									MgO
51D	45.8	44.5	5.4							---
51E	58.8	39.1	2.1							---
	CaO									MgO
52A	3.5	75.4	15.3							1.1
52B	93.5	4.2	0.8							
52C	91.0	7.5	1.2							
52D	79.8	17.2	1.0							
52E	80.3	18.2	1.3							
52A	82.6	5.6	2.2							
52B	92.6	3.7	1.0							
52C	90.0	6.3	---							
52A	88.8	7.9	1.0							
52B	98.6	2.5	---							0.6
52C	87.5	9.0	1.9							
52D	94.8	4.4	1.0							
52E	88.7	10.5	0.8							
52A	91.0	6.8	3.5							
52B	96.7	1.6	0.8							
52C	90.9	7.4	1.2							0.7
52A	94.8	2.7	1.0							
52B	95.8	1.2	1.4							
52C	95.2	1.4	1.2							
52D	95.4	2.7	0.6							0.9
52E	95.5	2.6	1.0							

ASSAY LOG
 JACKHAMMER SAMPLES

NO. HOLE
 LOCATION
 DESCRIPTION

PAGE 17

HOLE NO.	WEIGHT OF CORE	ASSAY OF CORE			WEIGHT OF SLUDGE	ASSAY OF SLUDGE			CALCULATED ASSAY				
		CaCO ₃	SiO ₂	R ₂ O ₃		CaCO ₃	SiO ₂	R ₂ O ₃	MgCO ₃	CaCO ₃	SiO ₂	R ₂ O ₃	MgCO ₃
H	129A	90.4	5.6	1.5									
	129B	91.5	6.6	0.7									
	129C	89.5	11.0	0.8									
	129D	96.5	4.2	0.4									
	129E	91.8	7.4	0.7									
	130A	92.2	6.3	0.6									
	130B	74.0	21.6	1.4									
	130C	75.0	21.9	1.1									
	130D	85.3	15.5	0.8									
	130E	87.6	11.3	0.9									
	131A	73.5	20.6										

Drilled 16' - No outtings returned after 5 feet.

1 B

DIAMOND DRILL SAMPLES

ASSAY LOG

NO. HOLE Diamond Drill Hole #1

LOCATION

DESCRIPTION

Sample Number	Weight of Core	ASSAY OF CORE				Weight of Sludge	ASSAY OF SLUDGE				CALCULATED ASSAY					
		CaCO ₃	SiO ₂	R ₂ O ₃	MgCO ₃		CaCO ₃	SiO ₂	R ₂ O ₃	MgCO ₃	CaCO ₃	SiO ₂	R ₂ O ₃	MgCO ₃		
0-5		94.1	4.2	0.7							94.1	4.2	0.7			
5-10																
10-15		88.7	5.0	0.4							88.7	5.0	0.4			
15-20		89.5	5.0	1.0							89.5	5.0	1.0			
20-25		72.7	24.3	2.4		A	74.7	17.6	0.9		81.1	16.4	1.7			
25-30		89.7	5.5	1.0		B	76.8	15.7	0.6		89.7	5.5	1.0			
30-35		88.0	10.2	1.0			Some samples not considered in corrected assay				88.0	10.2	1.0			
35-40		97.0	1.4	0.4	-1.0		93.6	4.4	1.5	0.5	97.0	1.4	0.4			
40-45		81.4	16.5	1.8	#1.0		96.2	12.0	0.9	0.4	92.5	4.6	1.5			
45-50		80.0	17.8	1.8	-1.0		92.5	6.8	1.0	0.8	86.0	12.0	0.9			
50-55		41.7	58.0	2.5			91.2	6.9	1.0		88.9	9.2	1.0			
55-60		87.6	10.5	1.6	-1.0		79.0	22.7	1.2		89.9	7.0	1.0			
60-65		33.2	68.0	3.6	-0.5		80.3	16.8	1.4		77.6	23.8	1.0			
65-70		87.8	30.3	3.2	#1.0		79.6	16.8	1.4		79.6	17.6	1.4			
70-75		28.7	67.2	4.4	-1.0		77.8	16.5	1.4		73.6	16.7	1.5			
75-80		44.0	52.5	3.8	-1.0		80.5	16.0	1.9		79.5	16.7	1.9			
80-85		61.0	55.8	1.5	-1.0		80.5	16.8	1.6		79.9	17.0	1.6			
85-90		80.2	16.3	2.3	-1.0		70.9	26.8	1.7		71.0	26.7	1.7			
90-95		39.4	67.9	1.8			70.8	26.0	2.0		68.2	26.56	2.0			
95-100		70.7	25.4	3.1	-0.5		79.5	17.2	2.0		78.4	19.5	2.1			
100-105		86.1	20.3	2.3	-0.5		71.0	25.3	2.4		70.1	24.8	2.48			
105-110		60.5	56.6	1.5			82.5	12.7	1.7		80.2	16.4	1.7			
110-115		74.2	35.0	3.6			No Sludge Return below this point				74.5	23.0	3.6			
115-120		63.1	41.3	2.1							68.1	41.5	2.1			
120-125		61.5	34.0	2.9							61.5	34.0	2.9			
125-130		55.6	32.8	1.3							56.6	32.8	1.3			
130-135		32.8	62.6	4.0							32.8	62.6	4.0			
135-140		70.2	31.5	1.6							70.2	31.5	1.6			
140-145		66.8	41.5	2.1							66.8	41.5	2.1			
145-150		45.9	45.3	3.9							45.9	45.3	3.9			
150-155		45.0	58.7	12.0	7.1						45.0	58.7	12.9	7.		
155-160		68.1	28.8	2.1							68.1	28.8	2.1			
160-165		87.0	10.5	1.2							87.0	10.5	1.2			

A S S A Y L O G

NO. HOLE Diamond Drill Hole #2

LOCATION

DESCRIPTION

Sample Number	Weight of Core	ASSAY OF CORE				Weight of Sludge	ASSAY OF SLUDGE				CALCULATED ASSAY			
		CaCO ₃	SiO ₂	R ₂ O ₃	MgCO ₃		CaCO ₃	SiO ₂	R ₂ O ₃	MgCO ₃	CaCO ₃	SiO ₂	R ₂ O ₃	MgCO ₃
0-5		95.6	6.2	0.5			87.8	10.6	1.2				90.9	
5-10		94.8	5.7	0.6			85.0	12.3	2.0				90.6	
10-15		91.8	6.4	0.8			93.8	3.5	1.0				95.0	
15-20		97.5	2.3	0.6			No Sludge						97.5	
20-25		95.6	2.4	0.6			No "						95.6	
25-30		94.8	3.6	0.5			92.5	2.6	4.5	1.1			95.4	
30-35		97.0	1.4	0.4	-1%		96.2	1.5	1.4				96.5	
35-40		85.7	12.6	1.0			87.8	9.8	-				87.1	
40-45		92.7	6.4	0.7			91.0	5.5	1.0				91.1	
45-50		93.8	4.7	0.6			88.1	10.1	0.6				89.2	
50-55		96.8	1.6	0.4			89.8	7.4	1.9				90.0	
55-60		97.6	1.6	0.8			95.4	2.0	3.0				95.5	
60-65		91.7	5.9	0.7			96.6	2.9	1.4				95.2	
65-68		90.9	1.6	0.7			92.9	5.2	1.7				93.8	
65-73		94.7	3.0	0.6			No Sludge						94.7	
73-74		95.6	2.4	0.6			No "						95.6	
74-76		95.2	2.5	0.6			No "						95.2	
76-80		96.6	2.3	0.6			93.5	2.6	6.0	1.1			94.1	
80-86		96.0	1.9	0.5										
85-90		No Core					92.2	5.1	2.6				92.2	
90-94		96.3	0.5	0.5			95.9	5.2	1.4				96.3	
94		92.3	5.9	0.7			95.5	2.9	1.1	0.7			95.4	
100-107		94.4	0.8	1.7			87.5	10.4	2.9	0.8			87.8	
107-112		96.6	1.8	0.4			86.2	11.5	2.7				86.6	
112-117		96.7	1.6	0.2			88.4	11.9	3.6	0.9			88.8	
117-122		97.7	0.7	0.3			93.8	5.5	2.4				93.9	
122-127		96.7	1.3	0.8			92.3	7.0	1.9				92.4	
127-132		81.6	17.4	1.0			95.2	5.7	2.9	1.2			94.0	
132-137		92.6	0.9	0.6			81.4	3.6	6.5	2.1			81.4	
137-142		96.6	2.3	0.5			86.4	8.9	1.4				88.6	

ASSAY LOG

Sample Number	Height of Core	ASSAY OF CORE				Weight of Sludge	ASSAY OF SLUDGE				CALCULATED ASSAY			
		CaCO ₃	SiO ₂	R ₂ O ₃	MgCO ₃		CaCO ₃	SiO ₂	R ₂ O ₃	MgCO ₃	CaCO ₃	SiO ₂	R ₂ O ₃	MgCO ₃
		NO. HOLE Diamond Drill Hole #2 LOCATION DESCRIPTION												
142-147		76.4	21.5	1.0		81.8	16.2	1.4		81.8				
147-152		76.6	21.5	1.1		81.2	3.5	0.6	1.4	80.6				
152-157		62.6	15.9	0.7		81.5	5.0	0.1		81.1				
157-162		37.1	1.6	0.4		87.8	9.6	1.4		88.2				
162-167		84.5	3.3	0.5		88.9	7.8	1.8		89.5				
167-172		30.0	66.5	2.5		82.8	12.2	2.8		80.6				
172-176		71.2	25.4	2.0		87.6	7.8	1.9		87.5				
176-182		65.8	27.8	2.0		69.0	28.4	3.2		69.0				
182-186		73.3	24.4	1.9		66.5	27.8	0.9		67.7				
186-191		61.3	36.2	2.0		60.0	14.7	1.1		78.0				
191-191 ¹		26.9	70.0	1.9		No	Sludge			26.9				
191 ¹ -200		51.5	49.7	2.6		72.2	14.5	10.9	1.8	71.6				
200-206		48.6	50.3	2.0		80.5	14.7	4.1		78.2				
206-207 ¹		32.0	65.2	2.0		No	Sludge			32.0				
207 ¹ -208		87.8	4.7	0.6						87.2				
208-208 ⁹		75.2	20.7	1.5						75.2				
208-211		94.1	2.4	0.9						94.1				
211-218		75.3	21.5	1.1						75.3				
218-218		67.8	29.4	1.5						67.8				
218-222		69.4	29.0	1.4		(83.6	4.1	2.6		86.7				
222-226														
226-230		59.2	37.7	1.5		79.4	14.5	4.9		70.9				
230-238		59.2	36.8	1.0		67.2	10.4	2.2		64.6				
238-238		37.4	59.6	1.8		80.0	17.1	2.0		70.1				
238-243		43.1	47.6	2.7		No	Sludge			46.1				
243-244		63.6	33.2	1.8		77.9	19.1	1.9	1	75.1				
244-249		42.9	65.3	2.5		72.3	22.5	3.2	1	68.3				
249-254		24.2	71.3	2.4		63.7	33.7	1.9	1	62.1				
254-259		56.0	41.3	3.5		59.6	28.2	1.7	0.6	59.4				
259-264		55.2	44.3	1.5		67.2	27.5	5.4	2.0	63.6				
264-271		No	Core			69.1	28.2	1.9	1	69.1				
271-276						55.5	37.0	3.9	2.4	55.5				

ASSAY LOG

NO. HOLE Diamond Drill Hole #3

LOCATION

DESCRIPTION

Sample Number	Weight of Core	ASSAY OF CORE				Weight of Sludge	ASSAY OF SLUDGE				CALCULATED ASSAY			
		CaCO ₃	SiO ₂	R ₂ O ₃	MgCO ₃		CaCO ₃	SiO ₂	R ₂ O ₃	MgCO ₃	CaCO ₃	SiO ₂	R ₂ O ₃	MgCO ₃
0-5		95.9	5.2	0.5										95.9
5-10		98.8	0.8	0.5		87.7	10.0	2.5	0.4					88.6
10-15		98.0	1.2	0.2		86.8	10.1	1.5						87.2
15-20		98.5	9.8	0.5		84.5	3.7	0.6						84.2
20-24	No Core					85.4	3.4	0.8						85.4
24-29	"					85.5	3.5	0.8						85.5
29-34		91.1	8.0	0.5		90.8	4.8	3.7						90.9
34-39		89.8	9.0	0.5		87.8	6.8	2.2						88.0
39-44		97.3	1.4	0.2		85.8	5.8	3.9						86.2
44-49		89.0	9.2	0.4		88.0	6.5	2.9						88.0
49-50		91.1	5.8	1.6	3.2	88.0	7.5	4.8	3.2					88.9
50-55		69.2	12.4	1.7	14.9	80.6	12.5	8.5						76.0
55-58 ¹		55.8	29.9	3.9		No	Sludge							55.8
58-60 ⁷		26.4	56.1	9.6	1.2	"	"							26.4
60 ⁷ -63		28.3	55.2	9.8		"	"							28.3
63-70		60.7	16.8	1.4		88.0	11.5	6.9						88.4
70-75		97.5	1.8	0.6		66.0	22.6	15.0	2.4					71.6
75-80		94.5	5.1	0.5		No	Sludge							94.5
80-84		96.6	2.8	0.4		71.0	18.0	10.4	1.3					76.1
84-89		75.6	22.9	0.8		90.4	9.4	1.8	1.7					87.4
89-91		97.6	1.8	0.5		83.8	13.9	1.5	-0.5					87.1
91-96		82.8	17.2	0.7		72.6	24.0	3.0	1.6					74.1
96-99		95.0	4.4	0.4		89.2	7.2	2.5	1.6					82.3
99-101 ¹		84.7	14.6	0.5		80.1	16.6	1.9	1.9					80.8
100 ¹ -105 ¹		94.2	5.1	0.5		No	Sludge							94.2
105 ¹ -107		61.9	35.7	3.1		"	"							61.9
107-112		91.3	7.2	1.1		"	"							91.3
112-116		74.0	25.0	1.0		67.3	30.9	1.8	0.5					66.6
116-126		76.2	22.9	1.0		70.5	27.7	0.9	0.5					70.6
126-130	No Core					88.8	6.7	2.1						88.8
130-134		40.1	58.4	1.0		75.4	22.9	1.2	-1.0					75.6

ASSAY LOG

NO. HOLE Diamond Drill Hole #3

LOCATION

DESCRIPTION

Sample Number	Weight of Core	ASSAY OF CORE				Weight of Sludge	ASSAY OF SLUDGE				CALCULATED ASSAY			
		CaCO ₃	SiO ₂	R ₂ O ₃	MgCO ₃		CaCO ₃	SiO ₂	R ₂ O ₃	MgCO ₃	CaCO ₃	SiO ₂	R ₂ O ₃	MgCO ₃
154-159		74.6	24.5	0.6		76.6	20.8	2.5	-1.0	76.6				
159-144	No Core					No Sludge								
144-149		66.0	12.2	0.5		74.2	24.5	2.8	1.0	77.5				
149-154		47.5	50.6	1.0		68.2	36.7	2.9	1.2	67.8				
154-157		55.6	45.0	0.6		62.0	30.5	5.5	2.0	61.6				
157-162		52.4	46.9	1.5		27.0	66.1	2.6	-1.5	28.0				
162-168		58.9	42.5	1.5		26.9	70.4	2.6	1.2	29.0				
168-174		75.7	25.6	0.6		No Sludge				75.7				

ASSAY LOG

NO. HOLE Diamond Drill Hole #4

LOCATION

DESCRIPTION

Sample Number	Weight of Core		Weight of Sludge				ASSAY OF SLUDGE				CALCULATED ASSAY					
	CaCO ₃	SiO ₂	R ₂ O ₃	MgCO ₃	CaCO ₃	SiO ₂	R ₂ O ₃	MgCO ₃	CaCO ₃	SiO ₂	R ₂ O ₃	MgCO ₃	CaCO ₃	SiO ₂	R ₂ O ₃	MgCO ₃
0-5	96.8	2.1	0.7		96.5	1.8	1.1	0.8	96.8							
5-10	94.8	3.9	0.4		88.2	3.9	1.3		88.6							
10-14	97.0	0.8	0.6		94.0	3.0	0.9		94.1							
14-18	96.3	1.3	0.6		95.2	1.6	1.5		95.4							
18-22	96.6	1.8	0.6		99.0	1.9	1.5		98.7							
22-26	95.2	2.0	0.8		89.9	2.7	1.5		90.9							
26-29	95.8	2.0	0.7		91.2	3.5	5.2	1.7	92.3							
29-34	92.7	5.6	0.8		93.2	4.0	4.2		92.9							
34-36	96.3	1.9	0.4		95.9	1.9	1.1		96.0							
36-40	95.6	2.3	0.8		96.5	1.4	2.0		96.6							
40-44	97.2	1.1	0.4		97.2	1.4	0.8		97.2							
44-48	97.8	1.4	0.5		97.3	1.0	0.9		97.3							
48-54	96.8	1.2	0.2		97.3	1.1	0.7		97.2							
54-59	98.8	1.4	0.4		No	Sludge			98.6							
59-62	96.5	1.5	1.3		85.5	12.8	2.6		85.8							
62-67	96.5	2.6	0.4		95.2	3.3	0.7		95.3							
67-72	98.2	1.5	0.4		94.6	3.3	1.0		94.6							
72-76	97.3	1.8	0.4		No	Sludge			95.2							
76-79	96.4	2.6	0.4		94.9	2.7	0.9		95.2							
79-84	98.7	2.6	0.5		95.2	2.3	1.9		95.2							
84-87	95.8	2.5	1.0		94.6	3.0	1.0		94.3							
87-92	96.5	2.4	0.7		95.5	2.2	1.5		95.4							
92-97	96.2	1.8	0.3		95.6	2.5	1.7		95.0							
97-102	96.3	1.6	0.4		96.3	2.0	1.3		96.3							
102-104	97.8	1.1	0.2		94.2	2.3	1.7		94.6							
104-109	97.8	1.6	0.3		89.5	5.6	2.0	3.0	90.0							
109-114	96.3	3.6	0.4		90.6	6.7	2.4		90.7							
114-119	91.8	7.2	0.6		87.8	7.2	3.1	1.8	88.0							
119-125	84.4	14.4	0.8		89.3	7.1	2.8	2.5	89.2							
125-130	80.4	17.8	1.0		No	Sludge			80.4							
130-134	90.5	9.0	0.5		80.0	7.1	2.1	1.5	80.0							

ASSAY LOG

NO. HOLE Diamond Drill Hole #4

LOCATION

DESCRIPTION

Sample Number	Weight of Core				Weight of Sludge	ASSAY OF SLUDGE				CALCULATED ASSAY			
	CaCO ₃	SiO ₂	H ₂ O ₃	MgCO ₃		CaCO ₃	SiO ₂	R ₂ O ₃	MgCO ₃	CaCO ₃	SiO ₂	R ₂ O ₃	MgCO ₃
134-139	91.1	7.8	0.5	-1%		89.8	6.9	2.1	1.5	89.9			
139-144	95.2	3.2	0.4	"		83.2	10.5	3.4	2.0	84.2			
144-149	97.2	1.2	0.3	"		85.3	10.3	3.2	2.0	86.0			
149-154	97.5	1.4	0.4	"		84.2	10.4	3.5	2.2	87.0			
-158	92.7	5.6	0.4	"		85.9	11.5	0.6		86.3			
158-162	98.0	1.0	0.3	"		86.7	10.2	0.6		87.5			
162-166	97.4	0.8	0.2	"		86.9	9.7	0.7		87.7			
166-171	No	Core				72.8	24.6	2.4		72.8			
171-176	"	"				78.6	18.4	0.5		78.6			
176-181	98.2	0.8	0.2	-1%		83.2	14.6	1.1		83.2			
181-185	No	Core				84.3	13.7	1.6		84.3			

ASSAY LOG

NO. HOLE Diamond Drill Hole No. 5

LOCATION

DESCRIPTION

Sample Number	Weight of Core	Weight of Sludge				Weight of Sludge	ASSAY OF SLUDGE				CALCULATED ASSAY			
		CaCO ₃	SiO ₂	H ₂ O	MgCO ₃		CaCO ₃	SiO ₂	H ₂ O	MgCO ₃	CaCO ₃	SiO ₂	H ₂ O	MgCO ₃
67	}					93.2	3.9	0.9	1.1	93.8				
6-15		97.5	1.0	0.3		93.5	4.0	0.5	1.4	93.5				
6-20						90.5	5.3	5.2	-1.0	90.5				
6-25		93.2	4.3	0.2		92.5	5.7	0.9	-1.0	92.5				
6-30		No Core				91.5	5.5	5.2	-1.0	91.5				
6-32					91.4	7.1	1.5	-1.0	91.3					
6-37	89.0	0.2	0.4		90.6	6.4	1.3		90.5					
6-42	No Core				89.2	8.3	1.0		89.2					
6-47	97.2	0.7	0.3		93.5	4.2	1.3		93.3					
6-52	97.3	0.4	0.1		91.7	5.9	1.5		91.3					
6-57	No Core				93.5	2.5	0.3		93.5					
6-62	96.5	1.0	0.2		61.8	9.5	7.8	1.6	82.1					
6-67	90.6	6.2	0.4		82.3	14.6	2.5		82.7					
6-71	93.0	3.3	0.6		85.7	12.0	2.0		86.0					
6-77	90.7	6.5	0.4		92.7	6.1	1.6		92.4					
6-82	96.0	1.9	0.3		89.5	7.5	2.4		89.6					
6-89	81.3	15.7	1.1		85.5	11.9	1.9		85.0					
6-94	74.3	22.2	1.3		68.6	31.4	1.6		67.6					
6-99	91.7	7.5	0.3		74.2	23.1	2.8		73.9					
6-104	89.3	7.3	0.3		79.3	18.7	1.7		80.1					
104-109	86.8	9.3	0.7		76.7	17.3	2.3		77.3					
109-114	91.2	22.3	1.3		65.5	11.6	2.4		64.7					
114-119	90.5	0.1	0.6		70.2	25.4	1.3		71.0					
119-124	92.9	25.6	1.0		76.1	21.5	0.9		75.3					
124-129	91.2	22.5	2.2		None				53.2					
129-134	84.7	12.7	1.1		72.5	22.7	1.4	0.7	73.0					
134-139	53.2	5.0	1.3		74.3	19.4	1.6	1.6	73.9					
139-144	90.7	22.3	1.3		63.7	25.5	1.1	0.9	73.7					
144-150	80.3	67.7	1.4		None				28.3					
150-155	60.0	30.1	1.3		64.3	30.7	4.3		64.3					

ASSAY LOG

NO. HOLE Diamond Drill Hole 25

LOCATION

DESCRIPTION

Sample Number	Weight of Core	ASSAY OF CORE				Weight of Sludge	ASSAY OF SLUDGE				CALCULATED ASSAY		
		CaCO ₃	SiO ₂	FeO	MgO		CaCO ₃	SiO ₂	FeO	MgO	CaCO ₃	SiO ₂	FeO
165-167	No Core					28.0	55.5	9.8	4.8	28.0			
167-161	" "					26.8	54.1	11.4	5.2	26.8			
161-164	" "					15.1	62.3	16.2	2.0	15.1			
164-169	" "					62.6	23.5	3.0	4.0	62.6			
169-174	28.1	9.3	0.9			50.9	29.1	4.0	4.6	64.1			
174-178	17.3	5.3	0.7			73.0	10.1	3.7	1.0	73.0			
178-182	76.3	21.9	0.8			75.3	16.2	2.4	2.6	75.4			
182-188	24.9	6.1	0.9			96.7	2.1	0.6		96.4			
188-193	15.7	10.0	0.5			95.3	1.7	1.3		92.2			
193-198	97.0	5.3	0.5			91.3	6.3	0.9		92.4			
198-204	88.7	10.4	0.4			90.3	6.5	1.4		90.7			
204-209	25.0	4.0	0.1			84.0	14.0	0.7		84.0			
209-214	91.0	7.3	0.1			83.4	15.1	0.8		83.7			
214-219	73.2	25.3	0.3			77.4	20.8	0.9		76.6			
219-224	70.1	26.3	0.3			76.0	22.3	0.3		75.7			
224-229	73.5	22.9	0.7			66.1	27.3	3.9	2.0	65.2			
229-234	No Core					77.3	16.9	2.1	1.7	77.3			
234-239	66.0	19.5	0.7			67.7	29.6	2.1		66.4			
239-244	36.2	62.3	0.3			71.9	26.1	2.4	2.0	70.5			
244-249	No Core					65.7	28.3	2.1		65.7			
249-254	74.0	24.2	0.3			71.0	27.3	1.5	1.2	71.1			
254-259	No Core					62.7	33.5	3.6		62.7			
259-262	" "					60.3	34.9	2.5	1.1	60.3			
262-267	" "					62.2	33.3	2.6	1.3	62.2			
267-272	" "					62.2	34.1	1.7	1.4	62.2			
272-279	46.7	50.2	1.0			67.4	28.2	2.0	1.4	66.2			
279-286	44.4	52.0	0.7			60.3	34.0	3.4	1.5	59.1			
286-294	55.2	40.7	0.3			61.7	34.0	2.9	1.5	61.5			
294-299	43.4	54.3	0.2			48.6	44.0	4.1	1.5	49.1			
299-302	No Core					61.3	43.8	2.6	1.4	52.9			

ASSAY LOG

NO. HOLE
LOCATION
DESCRIPTION

SAMPLE NUMBER	WEIGHT OF CORE	ASSAY OF CORE			WEIGHT OF M _g CO ₃ SLUDGE	ASSAY OF SLUDGE			M _g CO ₃	CALCULATED ASSAY			
		CaCO ₃	SiO ₂	Fe ₂ O ₃		CaCO ₃	SiO ₂	Fe ₂ O ₃		CaCO ₃	SiO ₂	Fe ₂ O ₃	MgO
302-309		71.5	28.3	0.8		59.5	35.0	4.0	2.4				59.5
309-314		85.6	12.7	0.5		57.2	40.1	1.4					61.1
314-318		70.4	21.0	0.6		57.2	39.2	1.8					60.9
318-323		63.8	34.5	0.5		54.4	40.4	4.0					54.0
323-328		62.5	56.6	0.7		53.8	41.0	2.2					54.0*
328-333		61.6	37.1	0.6			None						61.9
333-338		69.8	29.1	0.4		74.6	18.0	12.0					74.4
338-343			No Core			75.8	18.1	12.5					73.0
343-349		80.6	18.6	0.6		69.0	35.4	5.6					71.5*
349-356		65.1	32.4	0.8		48.3	47.0	2.9	1.7				49.0
356-357		89.2	68.2	0.8		47.7	45.4	4.4					46.6
357-362		65.6	51.7	0.6		66.5	26.9	3.4					68.2
362-368			None			47.6	38.3	8.4					47.6
368-374		87.2	11.5	0.5		79.9	15.3	2.7	1.8				81.2*
374-380		62.7	56.3	0.7		62.3	31.2	3.8	2.0				62.3
380-385		51.3	46.0	1.0		53.6	40.3	3.8	2.0				53.4
385-388		87.6	11.4	1.0		47.3	44.2	5.0	2.2				46.6
388-392			None			34.3	59.2	4.2					34.5
392-393			"			32.6	60.9	4.4	2.1				32.5
393-400		69.6	29.5	0.7		57.6	39.0	1.6	1.2				59.7*
400-402		66.6	53.0	0.7		57.6	59.1	1.3	1.1				57.1
402-409	1/4	57.8	40.4	1.2		55.2	39.2	3.3	1.9				56.4
409-414			None			56.6	38.0	4.2	1.8				56.6

ASSAY LOG

NO. HOLE
LOCATION
DESCRIPTION

SAMPLE NUMBER	WEIGHT OF CORE	ASSAY OF CORE			WEIGHT OF SLUDGE	ASSAY OF SLUDGE			CALCULATED ASSAY				
		CaCO3	SiO2	R2O5		CaCO3	SiO2	R2O5	CaCO3	SiO2	R2O5	MgCO3	
0-5					54.2	5.4	0.8						
5-10					55.1	4.0	0.6						
10-15					54.2	1.8	1.5						
15-20					52.8	6.6	0.6						
20-26					52.6	5.8	0.6						
26-32					53.5	7.7	1.8						
32-37					53.4	7.4	3.0						
37-42					53.5	6.4	2.6						
42-47					53.5	7.0	2.0						

ASSAY LOG

NO. HOLE
LOCATION
DESCRIPTION

SAMPLE NUMBER	WEIGHT OF CORE	ASSAY OF CORE			WEIGHT OF SLUDGE	ASSAY OF SLUDGE			CALCULATED ASSAY					
		CaCO ₃	SiO ₂	FeCO ₃		CaCO ₃	SiO ₂	FeCO ₃	CaCO ₃	SiO ₂	FeCO ₃	MgO		
145-145					65.7	55.6	1.8							
146-163					66.2	51.6	1.2							
153-153					64.8	52.6	1.2							
158-163					65.2	52.9	1.0							
165-163					71.2	54.5	5.6 *							
168-173					65.8	59.9	5.0							
175-173					67.5	58.8	2.0							
178-183					41.2	56.9	1.4							
183-186					24.8	70.8	2.7							
188-193					56.6	62.0	2.6							
193-196					25.2	72.1	2.0							
196-201					39.8	61.8	4.5							
201-206					47.5	48.2	0.5							
206-212					52.8	44.4	1.6 *							
212-217					62.5	18.4	3.8							
217-222					65.9	52.0	1.8							
222-229					62.0	12.8	5.2							
234-234					74.9	20.0	5.9							
234-239					78.0	17.6	4.0 * 1.4							
239-241								No Sludge						
241-246					42.8	57.2	2.8	1.2						
246-251					22.0	71.8	5.8							
251-258					57.2	56.6	4.9	1.0						
258-259					29.6	63.8	4.7	1.0						
259-264					68.7	11.4	8.2							
264-269					44.8	59.8	2.5							
269-274					58.5	37.4	5.5	1.3						
274-278					45.9	39.5	5.5							
278-283					62.5	54.9	2.6							
283-288					61.5	55.2	2.6	1.2						
288-292					59.8	36.0	2.9							

A S S A Y L O G

NO. HOLE Diamond Drill Hole 36A

L O C A T I O N

D E S C R I P T I O N

Sample Number	Weight of Core	A S S A Y O F C O R E				Weight of Sludge	A S S A Y O F S L U D G E				C A L C U L A T E D A S S A Y			
		CaCO ₃	SiO ₂	H ₂ O	H ₂ SO ₄		CaCO ₃	SiO ₂	H ₂ O	H ₂ SO ₄	CaCO ₃	SiO ₂	H ₂ O	H ₂ SO ₄
292-297						46.8	45.1	6.8						
297-303						48.8	48.8	6.4						
303-308						44.8	49.3	5.9						
308-313						87.2	28.4	3.0						
313-317						67.5	27.5	3.5						
317-324						26.0	5.9	2.5						
324-329						65.2	30.0	4.9						
329-334						63.2	30.0	5.6						
334-340						62.5	30.1	5.0						

ASSAY LOG

NO. HOLE
LOCATION
DESCRIPTION

SAMPLE NUMBER	WEIGHT OF CORE	ASSAY OF CORE			WEIGHT OF MgCO ₃ SLUDGE	ASSAY OF SLUDGE			CALCULATED ASSAY				
		CaCO ₃	SiO ₂	R ₂ O ₃		CaCO ₃	SiO ₂	R ₂ O ₃	MgCO ₃	CaCO ₃ -SiO ₂	R ₂ O ₃	MgCO ₃	
0-5		No Core				37.9	60.2	1.8					
5-8		38.6	61.7	0.8		26.4	72.0	1.1					
9-12		No Core				20.4	77.8	1.2					
12-14		37.7	59.3	0.9		22.8	76.3	1.3					
14-17		15.5	52.3	1.0									
14-18		24.9	72.0	1.2		29.5	68.8	1.2					
14-20		40.3	57.3	0.9		49.7	47.8	1.2					
19-27		55.2	42.5	1.0		46.7	48.7	1.7					
27-30		56.2	41.3	0.8									
30-32		60.2	58.2	0.4		70.3	27.3	1.2					
32-35		46.0	50.3	0.5		51.6	36.8	3.0 *					
35-34		66.0	32.0	0.6		No Sludge							
34-37		59.7	40.1	0.7		60.9	16.5	2.4					
37-42						38.4	11.1	1.4					
42-47		No Core				37.9	13.6	1.0					
47-52		"				81.5	18.1	1.1					
52-55		"				75.7	21.9	1.1					
55-60		"				60.3	9.4	2.6					
60-73		"				No Sludge							
73-74						71.3	24.2	4.6 *	1.9				
74-77		22.4	75.6	0.8		No Sludge							
77-82		No Core				47.3	51.6	1.1					
82-86		"				54.6	64.4	1.0					
86-91		"				39.4	59.5	1.1					
91-96		"				37.6	60.9	1.2					
96-101		"				40.0	59.5	1.0 *					
101-106		"				91.5	6.8	1.1					
106-111		"				59.4	39.9	1.2					
111-116		86.5	13.3	0.5		68.7	38.4	1.9					
116-121		95.4	4.4	0.3		73.3	24.7	1.0					
121-126		91.0	6.3	0.3		53.3	30.0	1.3					
126-131		96.2	3.9	0.1		65.4	30.7	1.1 *					

ASSAY LOG

NO. Hole Diamond Drill

LOCATION

DESCRIPTION 7A

ASSAY OF SLUDGE CALCULATED ASSAY

Sample Number	Weight of Core	Weight of Sludge				ASSAY OF SLUDGE					CALCULATED ASSAY				
		CaCO ₃	SiO ₂	R ₂ O ₃	MgCO ₃	CaCO ₃	SiO ₂	R ₂ O ₃	MgCO ₃	CaCO ₃	SiO ₂	R ₂ O ₃	MgCO ₃		
131-135)	1	96.5	3.0	0.1		96.5	2.8	0.6							
136-141)	18					95.2	3.4	0.5							
143-146		97.2	1.7	0.2		95.4	3.6	0.4							
146-151		No Core				94.5	2.0	0.4							
151-156		-----				95.3	4.2	0.5							
156-161		-----				91.8	4.5	--							
161-166		-----				92.9	4.4	1.9							
166-171		-----				92.8	4.5	1.2							
171-176		-----				90.0	7.8	0.9							
176-181		96.7	1.8	0.2		94.5	3.6	2.4							
181-186		No Core				92.8	4.2	2.3							
186-191		-----				92.1	5.0	1.2							
191-196		-----				No Sludge									
196-201		-----				96.3	2.8	0.6							
201-206		-----				92.8	6.8	0.8							
206-211		-----				92.0	7.2	0.8							
211-216		-----				90.4	8.3	0.8							
216-221		94.2	3.2	0.5		87.0	9.2	3.8							
221-226		No Core				81.0	14.8	3.5							
226-231		83.7	14.2	0.4		No Sludge									
231-236		95.1	3.8	0.6		86.2	9.8	3.4							
236-241		No Core				90.6	5.7	3.4							
241-246		No Core				88.6	7.4	2.6							
246-251		96.0	1.6	0.4											
251-259		No Core													

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ASSAY LOG

NO. HOLE Diamond Drill Hole No. 9

LOCATION

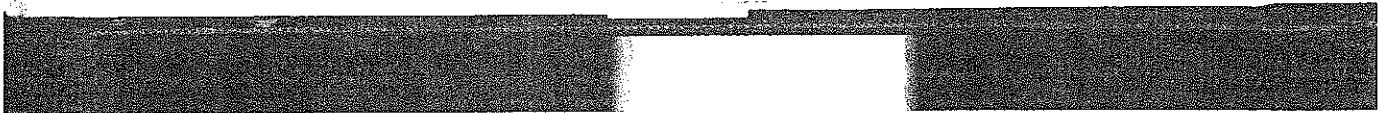
DESCRIPTION

Sample Number	Weight of Core	ASSAY OF CORE				Weight of Sludge	ASSAY OF SLUDGE				CALCULATED ASSAY			
		CaCO3	SiO2	R2O3	MgCO3		CaCO3	SiO2	R2O3	MgCO3	CaCO3	SiO2	R2O3	MgO
0-5		97.0	1.2	0.4		59.7	26.1	8.5						
5-10		95.6	2.9	0.2		80.7	11.0	5.2						
10-15)		96.9	1.4	0.2		96.0	2.0	2.0						
15-19)						97.5	1.7	0.5						
19-23		97.0	1.4	0.1		97.5	1.6	1.1						
23-28		96.4	1.7	0.3		86.5	6.8	4.6						
28-32		98.2	1.3	0.5		95.2	2.0	3.0						
32-37						97.5	1.6	1.0						
37-42						96.5	2.2	2.6						
42-47						No Sludge								
47-53						87.0	10.1	2.2						
53-58						66.3	29.2	1.2						
58-63						82.5	5.8	2.9						
63-65						93.5	3.8	1.5						
65-70						95.5	1.9	1.9						
70-74						94.3	2.0	3.0						
74-78						96.7	2.1	0.7						
78-84						97.2	2.0	0.7						
84-89						92.8	4.8	0.9						
89-94						93.4	4.4	1.0						
94-100														
100-103														
103-108														
108-113														
113-119						85.0	13.3	1.2						
119-123														
123-128						85.6	12.8	1.4						
128-131														
131-139						84.0	13.5	2.6						

1 c

HAND SAMPLES

TABULATIONS OF ANALYSES OF THE SURFACE CLAYS TO DATE



TRANSCRIPT OF ANALYSIS OF CLAY BORER HOLE
 Permanents Project
 Area A

Sample No.	Basic	SiO	Al O	Fe O	CaO	MgO	Undet.	% Coarse Waste	
1	0-6'	Ignited	66.0	14.1	7.7	1.0	4.3	6.9	59.
1	5'-6'6"	"	62.0	19.5	5.7	0.9	4.0	7.5	59.
2	0-5'3"	"	50.5	17.2	15.7	3.4	4.6	6.6	74.
4	0-5'	"	60.9	13.5	3.2	1.4	9.0	2.2	49.
6	0-5'	"	70.5	19.0	3.9	1.2	2.2	3.4	45.
6	5'-8'6"	"	57.4	23.4	8.5	2.3	3.7	4.7	70.
7	0-5'	"	54.6	30.7	10.0	0.8	3.7	0.2	79.
7	5'-10'	"	57.5	19.4	9.1	0.6	4.3	9.1	65.
9	0-5'11"	"	60.0	21.7	8.0	0.9	4.3	4.0	67.
11	0-5'	"	69.6	14.4	11.4	0.7	1.9	2.0	91.
12	0-5'	"	56.9	25.8	3.0	0.8	3.9	4.0	52.
12	5'-7'2"	"	58.2	23.0	7.4	0.4	3.9	7.1	54.
19	0-5'	"	58.5	25.1	6.9	0.9	3.4	5.1	74.
19	5'-10'	"	57.2	25.2	8.6	0.8	3.4	4.8	68.
21	0-16"	"	61.8	23.4	6.9	1.9	2.8	3.2	44.
31	0-3'	"	68.5	20.1	4.7	0.7	2.2	3.0	47.
36	0-3'	"	69.0	19.5	4.3	1.0	2.3	3.9	42.
38	0-3'6"	"	69.2	19.7	4.6	0.9	2.1	4.5	61.
40	0-5'0"	"	69.7	18.2	4.7	0.9	2.2	4.3	50.
41	0-4'6"	"	68.0	19.2	4.7	1.0	2.3	4.8	58.
43	0-5'	"	68.3	18.5	4.1	0.8	1.9	4.9	33.
43	5'-10'	"	66.7	19.3	6.0	0.8	2.1	5.9	38.
43	10'-11'2"	"	66.2	20.1	5.4	0.9	2.3	5.1	41.
51	0-5'	"	59.0	24.8	7.4	0.7	3.4	4.7	65.
51	5'-8'9"	"	57.7	14.6	14.0	0.4	6.7	6.8	53.
61	0-4'	"	65.3	19.4	7.7	1.4	2.6	3.3	26.
62	0-4'6"	"	67.9	19.9	4.5	0.9	2.5	4.3	54.
70	0-2'0"	"	69.2	18.5	4.5	0.9	2.2	4.7	43.
77	0-5'	"	59.4	25.1	3.3	0.6	3.4	4.2	62.
81	0-4'	"	71.4	17.3	4.0	1.1	1.6	4.6	43.
83	0-5'7"	"	72.5	18.3	3.8	0.6	1.5	3.3	31.
85	5'-10'	"	72.5	17.9	3.7	0.6	1.7	3.8	23.
98	0-5'	"	68.2	18.7	4.2	1.9	2.0	5.0	33.
98	5'-6'4"	"	66.6	20.4	5.1	1.0	2.3	4.0	73.
106	0-5'5"	"	68.5	18.3	5.8	1.2	2.4	3.8	45.
111	0-5'2"	"	67.1	21.3	3.5	1.4	2.4	4.3	29.
114	0-5'5"	"	63.7	20.9	3.6	1.5	3.5	2.6	22.
116	0-4'	"	56.2	20.4	13.7	3.4	4.8	1.5	47.
121	0-5'	"	69.2	13.3	5.3	1.6	2.3	3.3	44.
121	5'-10'	"	62.6	19.5	16.6	4.2	5.2	1.7	50.
121	10'-14'	"	62.4	19.1	16.1	5.1	5.4	1.9	42.
122	0-5'	"	59.4	19.7	11.2	2.4	5.0	2.3	19.
122	5'-6'6"	"	65.3	17.6	9.7	1.6	4.5	1.4	37.
124	0-5'	"	60.3	20.1	5.3	0.7	2.4	5.2	20.
126	0-5'	"	66.0	18.7	7.3	1.6	5.8	0.6	52.
137	0-5'	"	54.4	16.2	3.4	0.9	1.5	3.6	53.
137	5'-11'	"	66.0	19.9	6.5	1.0	2.8	3.8	34.
143	0-3'9"	"	69.9	18.8	4.6	0.9	1.9	3.9	56.
147	0-1'8"	"	60.4	21.4	4.6	0.7	2.4	4.5	49.
150	0-5'6"	"	68.7	10.2	5.3	1.3	2.3	3.2	38.
150	5'6"6'9"	"	59.5	18.4	3.0	0.9	2.1	4.1	34.
152	0-3'6"	"	68.4	19.7	4.8	0.8	1.9	4.4	30.

Sample No.	Description	%oxide						
		SiO	Al O	Fe O	CaO	MgO	Undet.	Waste
RI 188 0-4' 2"	Ignited	68.4	18.8	4.8	0.7	3.4	3.9	48.
189 0-4'	"	68.2	18.5	4.6	0.8	2.5	4.4	48.

ANALYSIS OF CLAY SAMPLES

AREA NO. B

Sample No.	SiO ₂	Al ₂ O ₃	Fe ₂ O ₃	CaO	MgO	Undeter- mined	Percentage of Coarse Material (Rejected)
BH 173A	54.3	17.4	14.2	3.4	7.9	2.8	46
173B	53.8	17.2	14.8	2.9	7.3	4.0	41
174	57.4	17.9	10.6	3.1	7.7	3.3	38
175	62.3	16.3	10.6	1.3	4.1	5.4	42
176	58.1	16.5	13.4	2.2	6.5	3.3	36
177	57.3	15.8	9.9	3.0	10.7	3.3	44
178A	67.3	17.2	6.8	0.9	2.6	5.2	57
178B	62.6	20.4	8.2	0.9	3.1	4.8	53
179A	70.4	17.1	4.8	1.2	2.2	4.3	34
179B	72.9	14.9	4.7	1.1	1.3	5.1	36
179C	70.6	15.4	6.4	0.8	2.0	4.8	37
180	74.6	14.8	3.9	0.7	2.1	3.9	24
181	70.5	16.9	4.7	0.7	2.4	4.8	39
182	66.8	19.2	4.8	0.8	2.3	4.1	52
183A	68.7	17.6	5.0	1.8	3.2	3.7	39
183B	69.3	20.6	1.8	1.3	4.0	3.0	26

ANALYSIS OF CLAY SAMPLES

AREA NO. B

Sample No.	SiO ₂	Al ₂ O ₃	Fe ₂ O ₃	CaO	MgO	Undeter- mined	Percentage of Coarse Material (Rejected)
BH 225	72.8 68.7	18.9	2.6	1.1	2.3	6.4	41
226	69.7	18.4	3.5	1.0	1.8	5.6	35
227	66.5	19.6	5.0	1.6	2.4	4.9	40
228	64.2	21.1	4.7	1.4	2.8	5.8	29
229	69.7	16.1	5.0	2.6	2.0	5.6	46
230	68.8	18.9	3.6	1.4	2.1	4.2	40
231	72.7	16.8	3.9	0.2	2.1	4.3	38
232	71.7	16.2	5.2	1.1	2.0	3.8	19
233	59.0	18.7	13.7	0.7	6.1	3.8	41
234	58.0 53.5	21.6	13.7	1.9	5.6	3.7	50
235	47.7	18.5	14.1	7.8	8.6	3.3	47
236	53.9	19.2	13.3	3.2	7.6	2.7	42
237	56.4	17.4	15.5	2.1	6.2	2.4	43
238	54.4	19.6	12.4	2.6	7.6	3.4	30
239	58.0	19.0	11.1	2.1	5.8	4.0	40
240	54.2	17.2	12.5	5.3	8.1	2.5	32
241	58.2	19.4	11.7	2.2	6.0	2.5	21
242	58.9	18.2	11.2	2.8	5.1	3.8	34
243	58.4	18.0	12.0	1.9	6.1	3.6	32
244	57.1	15.6	9.8	4.3	6.6	6.4	32
245	58.2	17.8	13.4	2.3	6.4	1.9	21
246	52.4	20.7	12.6	2.5	7.7	4.1	41

ANALYSIS OF CLAY SAMPLES

AREA NO. B

-2-

Sample No.	SiO ₂	Al ₂ O ₃	Fe ₂ O ₃	CaO	MgO	Undeter- mined	Percentage of Coarse Material (Rejected)
BH 247	53.2	19.1	12.5	3.6	7.3	4.3	36
248	58.5	18.0	11.9	1.7	5.2	4.7	36
249	57.4	20.6	12.9	1.7	*	7.4	28
250	67.1	19.5	4.9	0.9	*	7.6	35
251	71.5	15.7	4.7	1.3	*	6.8	37
252	No clay - all rock						
253	69.6	17.1	6.1	0.4	2.5	4.3	31
254	69.8	15.7	5.6	1.1	*	7.8	33
255	73.2	13.2	4.6	1.0	*	8.0	
256							
257	68.2	19.5	4.1	0.8	2.0	5.4	30
258	70.3	17.4	3.6	1.4	2.3	5.0	54
259	No clay - all rock						
260	63.2	17.8	10.0	2.1	3.6	3.3	45
261	56.4	19.0	12.0	2.4	6.9	3.3	41
262	62.2	16.5	9.1	2.5	7.4	2.3	36
263	60.5	17.2	9.2	4.7	4.9	3.5	27
264	47.6	13.2	10.5	12.8	14.7	1.2	26
265	52.7	20.4	14.3	3.9	7.7	1.0	40
266	51.8	19.0	14.7	4.6	7.5	2.4	42
267	70.2	17.9	4.2	0.8	2.0	4.9	46
268	68.2	18.1	7.9	0.2	2.7	2.9	43
269 <i>63.4</i>	60.1	18.9	13.1	2.7	4.5	0.7	35

(*) Range 2 - 6%

ANALYSIS OF CLAY SAMPLES

AREA NO. B

-3-

Sample No.	SiO ₂	Al ₂ O ₃	Fe ₂ O ₃	CaO	MgO	Undeter- mined	Percentage of Coarse Material (Rejected)
BH 270	54.8	17.7	15.2	4.5	7.6	0.2	48
271	51.8	19.3	14.1	3.9	8.9	2.0	38
272	68.5	18.0	5.4	1.3	2.7	3.1	31
273	54.1	18.9	12.7	4.2	6.3	3.8	43
274	49.6	18.1	15.2	4.9	9.4	2.8	60
275	52.4	18.9	16.7	4.0	1.9	6.1	35
276	69.7	17.6	3.4	1.7	2.1	5.5	31
277	69.7	17.9	4.6	0.8	2.2	4.8	35
278	70.3	15.4	4.1	1.4	2.2	6.6	45
279 73.8	72.4	16.3	5.3	0.9	1.9	3.2	24
280	51.1	17.5	12.7	4.3	10.0	4.4	53
281	53.0	17.1	15.5	4.8	8.2	1.4	57
282	56.2	18.1	12.6	4.6	7.2	0.3	25
283	45.7	15.2	14.7	8.8	15.7	-	36
284							
285	61.3	17.2	10.9	3.0	5.3	2.3	35
286	72.3	14.1	3.8	1.3	1.6	6.9	29
287							
288	71.9	16.3	3.5	1.4	1.8	5.1	40
288B	71.4	17.6	3.6	1.1	2.1	4.2	32
289							
290	55.2	16.6	14.0	4.7	7.5	2.0	59

ANALYSIS OF CLAY SAMPLES

AREA NO. F

-4-

Sample No.	SiO ₂	Al ₂ O ₃	Fe ₂ O ₃	CaO	MgO	Undeter- mined	Percentage of Coarse Material (Rejected)
BH 291							
292	57.2	17.2	11.5	3.2	6.8	4.1	22
293	51.3	18.1	14.7	6.4	6.8	2.7	45
294	50.1	17.8	13.6	4.8	10.2	3.5	64
295	55.0	18.9	13.1	2.4	5.6	5.0	47
296A	74.1	14.7	4.0	0.7	1.5	5.0	29
296B	64.3	17.2	9.1	1.9	4.1	4.4	26
297	51.7	17.8	12.8	3.7	11.0	3.0	55
298	54.4	16.5	13.0	4.8	8.4	2.9	49
299	54.6	17.7	12.5	3.1	7.3	4.8	34

ANALYSIS OF CLAY SAMPLES
 AREA NO. B

-5-

Sample No.	SiO ₂	Al ₂ O ₃	Fe ₂ O ₃	CaO	MgO	Undeter- mined	Percentage of Coarse Material (Rejected)
BH 326	70.1	17.7	4.5	0.9	2.3	4.5	55
327	70.1	18.5	4.9	0.5	2.3	3.7	36
328	66.3	20.2	5.0	0.9	2.9	4.7	46
329 <i>76.2</i>	68.8	18.2	4.9	1.5	2.3	4.3	55
330	68.8	20.4	1.5	1.1	2.3	6.9	63
331	69.0	17.9	4.6	1.3	2.4	4.8	47
332	71.5	17.8	1.9	1.3	1.7	5.8	62
333	70.3	16.8	4.0	1.5	2.0	5.4	57
334							
335	69.5	17.1	3.0	1.3	2.2	6.9	49
336	71.2	17.1	3.3	1.1	1.8	5.5	51
337	72.6	16.7	3.5	1.7	1.5	4.0	31
338	73.2	16.8	3.4	0.3	1.5	4.8	26
339	73.5	15.0	4.8	1.1	1.5	4.1	28
340 <i>76.6</i>	73.4	17.0	3.2	1.1	1.6	3.7	50
341	69.2	17.7	4.3	1.0	2.4	5.4	37
342							
343							
344							
345							
346							
347							

ANALYSIS OF CLAY SAMPLES

AREA NO. C

Sample No.	SiO ₂	Al ₂ O ₃	Fe ₂ O ₃	CaO	MgO	Undeter- mined	Percentage of Coarse Material (Rejected)
BH 193	53.2	19.0	14.0	3.2	8.8	1.8	45
194	60.6	20.3	9.6	1.9	5.0	2.6	37
195	47.7	19.9	15.0	9.9	3.3	4.2	42
196	54.7	18.1	14.1	2.6	9.1	1.4	40
197	56.8	19.0	13.2	4.1	6.2	0.7	38
198	58.1	15.1	15.2	1.4	9.3	0.9	45
199	53.7	17.1	15.8	4.1	8.2	1.1	38
200	62.3	16.7	11.0	1.5	5.3	3.2	39
201	63.6	17.1	9.8	1.0	5.4	3.1	48
202	64.5	19.0	11.4	1.2	2.8	1.1	32
203	61.7	15.0	14.6	1.8	3.9	4.0	38
204	69.5	14.2	10.6	1.6	2.2	1.9	35
205	69.3	18.6	8.6	0.8	1.5	1.2	46

596

10.8

ANALYSIS OF CLAY SAMPLES

AREA NO. C

Sample No.	SiO ₂	Al ₂ O ₃	Fe ₂ O ₃	CaO	MgO	Undeter- mined	Percentage of Coarse Material (Rejected)
BH 300	61.0	19.8	9.3	1.3	4.7	4.9	40
301	71.0	17.1	5.1	0.4	2.1	4.3	38
302	69.9	16.2	6.1	2.4	1.8	3.6	33
303	63.5	19.1	7.5	1.2	1.9	6.8	45
304	70.5	17.8	5.6	0.5	2.2	2.4	24
305	52.4	19.8	16.6	4.7	3.7	2.8	61
306	55.3	20.5	12.8	1.7	6.8	2.9	20
307	65.4	17.8	10.7	1.7	2.6	2.8	22
308	70.9	14.1	10.0	0.3	1.9	2.8	48
309							
310	59.3	18.2	13.8	2.2	4.8	1.7	45
311	51.7	22.3	16.9	3.3	4.2	1.6	40
312	50.8	21.0	15.2	7.4	4.7	0.9	38
313	48.7	21.8	18.3	4.4	4.9	1.9	60
314	71.8	16.8	8.7	0.7	1.1	0.9	64
315	69.2	17.7	10.1	0.8	1.3	0.9	43
316	58.0	20.6	14.0	0.3	5.1	2.0	25
317	60.5	18.7	11.9	0.4	3.5	5.0	31

ANALYSIS OF CLAY SAMPLES

AREA NO. C

-2-

Sample No.	SiO ₂	Al ₂ O ₃	Fe ₂ O ₃	CaO	MgO	Undeter- mined	Percentage of Coarse Material (Rejected)
BH 350	71.2	16.7	4.8	1.3	1.5	4.5	37
351	72.4	16.4	5.0	0.9	1.7	3.6	25
354							
355	71.2	16.2	4.7	1.4	2.2	4.3	46

ANALYSIS OF CLAY SAMPLES

AREA NO. D

Sample No.	SiO ₂	Al ₂ O ₃	Fe ₂ O ₃	CaO	MgO	Undeter- mined	Percentage of Coarse Material (Rejected)
BH 184 ⁵⁷	52.5	19.7	13.7	3.4	8.1	2.6	60
185 ⁵⁶	52.1	16.5	17.5	2.7	10.2	1.0	44
186 ⁷⁹	71.7	13.9	8.0	1.3	2.9	2.2	63
187A	59.9	18.6	12.0	1.2	4.7	3.6	32
187B ^{65.5}	61.9	17.7	10.4	1.2	5.8	3.0	48
187C	58.0	15.9	10.3	5.1	8.9	1.8	33
188	60.1	19.6	9.4	0.4	6.3	4.2	54
189A } ⁷⁵	70.0	15.5	9.1	0.9	2.3	2.2	39
189B }	68.4	16.9	9.2	0.2	2.3	3.0	31
190	56.4	23.8	12.0	4.9	2.3	0.6	35
191 ⁶⁸	59.4	22.1	10.9	3.9	2.8	0.9	30
192	58.8	19.4	11.5	2.2	6.8	2.1	51

60.7

11.16

TABULATION 3.

Analyses of Andesite and Associated Sandstone Formation.

(A) Upper Andesite.

(B) Franciscan sandstone and Shale along West
Limestone Contact.

(C) Interbedded Franciscan Sandstone and Shale.

TABULATION 3.

Analyses of Andesite and Associated Sandstone Formation.

(A) Upper Andesite.

(B) Franciscan sandstone and Shale along West
Limestone Contact.

(C) Interbedded Franciscan Sandstone and Shale.

UPPER ANDRESTER

(Jachhammer Samples)

	SiO ₂	Al ₂ O ₃	Fe ₂ O ₃	CaO	MgO
JH 27	55.0		28.2	1.9	0.3
JH 65A	53.8	14.2	11.6	3.8	11.9
JH 65B	51.2	14.0	11.4	7.2	12.2
JH 65C	48.0	14.1	10.8	10.6	11.6
JH 65D	46.6	14.2	10.9	17.0	9.6
JH 65E	42.6	14.2	10.5	25.8	8.6

Lower Andrester

	SiO ₂	Al ₂ O ₃	Fe ₂ O ₃	CaO
	52.0	14.0	11.0	1.0
	50.0	14.0	10.0	2.0
	48.0	14.0	10.0	14.0
	46.0	14.0	10.0	1.0

Dr. Fredrick F. ...

Drill No. A

	SiO_2	Al_2O_3	Fe_2O_3	CaO	MgO
54-47	11.5	11.7	10.1	1.2	7.8
Franciscan Sandstone and Shales along West Idanha Contact					
(Eachsummer Samples)					
54-47A	12.1	11.7	10.1	1.2	7.8
55-48	81.0	Al_2O_3	Fe_2O_3	CaO	MgO
JH 1522	54.1	15.7	11.5	5.5	6.7
JH 1523	55.5	17.8	12.5	5.8	6.8
JH 1524	52.5	17.5	13.7	2.8	5.3
JH 1525	46.1	10.0	7.0	51.4	3.1
JH 1526	49.2	11.1	8.0	10.2	2.8
JH 1527	56.7	17.2	15.4	6.2	5.0
JH 1528	46.7	14.5	13.4	15.2	4.7
JH 1529	45.2	15.8	14.1	10.0	6.5
JH 1530	47.8	16.9	13.7	12.5	4.8
JH 1531	48.2	17.5	14.7	9.5	5.2
JH 1532	51.8	17.0	14.2	4.5	6.5
54-47B	12.1	11.7	10.1	1.2	7.8

Drill No. B

	SiO_2	Al_2O_3	Fe_2O_3	$MgCO_3$
54-47C	12.2	1.5	10.1	1.0
54-47D	17.0	3.5	12.5	2.4

Drill No. C

54-47E	12.4	1.7	9.7	14.8
54-47F	11.1	1.1	8.1	11.5

Interbedded Franciscan Sandstone and Andesite

Diamond Drill No. C

	SiO_2	Al_2O_3	Fe_2O_3	CaO	MgO
60-65	48.3	15.8	10.8	16.8	7.6
70-74	50.1	16.7	9.8	12.4	8.8
74-78	48.3	15.2	9.6	15.3	8.8
80-83	46.3	15.3	9.6	12.4	8.6
83-88	47.2	19.6	12.6	8.8	10.6
93-98	46.4	17.7	10.9	6.9	9.2
98-104	48.0	18.7	11.7	6.9	10.3
110-116	49.6	18.8	11.6	6.7	11.9

Diamond Drill No. H

161-164	62.5	12.2	6.0	13.1	2.8
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Churn Drill Hole W-1

169-182	39.8	7.7	4.6	21.7	2.2
183-196	49.0	10.8	4.4	14.7	1.2

Churn Drill Hole W-3

263-272	35.8	3.0	2.8	50.5	0.6
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Diamond Drill Hole No. E

	SiO_2	R_2O_3	$CaCO_3$	$MgCO_3$
264-271	29.2	1.8	68.1	1.0
271-278	27.0	3.9	55.5	2.4

Diamond Drill Hole No. B

50-55	12.4	1.7	69.2	14.2
56-60	56.1	9.6	26.4	1.2

4 A

ANALYSES OF BAY CLAYS — POLAND HAND SAMPLES

TRANSCRIPT OF POLLAND HAND SAMPLES OF CLAYS
 Permanente Project

	SiO ₂	Al ₂ O ₃	Fe ₂ O ₃	CaO	MgO	Undet.	%Coarse Waste
P 1	61.0	20.4	7.7	2.2	4.6	4.1	
P 2	62.5	19.4	7.9	2.2	3.9	4.1	
P 3	62.3	18.8	8.3	1.4	4.3	4.9	
P 4	61.2	20.6	8.6	1.1	3.9	4.6	
P 5	62.5	19.4	8.4	1.3	3.9	4.5	
P 6	63.1	19.7	8.3	0.3	4.5	4.1	
P 7	56.4	15.5	6.6	3.3	8.5	4.7	
P 8	59.6	20.4	9.3	1.4	4.4	4.9	
P 10	58.3	17.5	12.5	4.6	4.9	1.7	
P 17	66.1	16.0	8.1	2.7	3.4	3.7	
P 18	58.7	16.2	14.9	3.3	4.7	2.2	

A B

LOGS OF WELLS EAST OF THE BAYSHORE HIGHWAY

WELL NO.	Owner	Log
1	Lowe & Lowe, Monte Vista	6 - 15 soil 15 - 306 yellow clay
2	Vidovich & Caviglia, Collins Ave., Sunnyvale	0 - 3 soil 3 - 55 clay 55 - 55 gravel 55 - 110 sand & gravel
3	A. G. Rose, Grant Rd. and Portland Ave.	0 - 20 clay & gravel 20 - 85 soft clay 85 - 90 red clay 90 - 95 gravel 95 - 140 soft red clay
4	Lewis Co., Ranch 8, Agnew Rd. near Bayshore Highway	22 - 55 blue clay 55 - 59 fine gravel 59 - 100 blue clay
5	Machado Wall, Mtn. View, Alviso Rd.	0 - 11 soil 11 - 13 sand & gravel 13 - 177 blue clay
6	Tompkins, Bayshore Highway & Jagels Rd.	0 - 9 adobe 9 - 13 yellow clay 13 - 18 yellow sand 18 - 49 blue clay 49 - 55 fine gravel 55 - 67 yellow clay 67 - 172 blue clay
7	H. Mitarai, Freitas Dairy Ranch	0 - 5 soil 5 - 60 yellow clay 60 - 111 sandy blue clay
8	Y. Oku, Mtn. View & Alviso Rd.	0 - 20 soil 20 - 30 yellow clay & gravel 30 - 60 yellow clay 60 - 115 yellow clay & gravel
9	U. S. Air Base - (old well)	0 - 8 top soil 8 - 24 blue clay 24 - 29 gravel 29 - 87 blue clay 87 - 112 yellow clay
10	Poncini, Mtn. View - across Bayshore Highway from Air Base	0 - 10 top soil 10 - 13 sand 13 - 65 yellow clay & gravel 65 - 85 gravel & clay 85 - 167 blue clay

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